

TPS56x200 采用 SOT-23 封装的 4.5V 至 17V 输入，2A/3A 同步降压稳压器

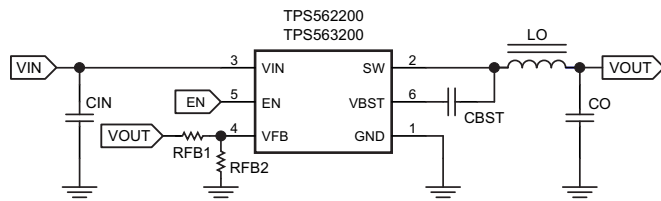
1 特性

- D-CAP2™ 模式控制，具有 650kHz 开关频率
- 输入电压范围：4.5V 至 17V
- 输出电压范围：0.76V 至 7V
- 集成 122mΩ 和 72mΩ 场效应晶体管 (FET) ('562200)
- 集成 68mΩ 和 39mΩ FET ('563200)
- 高级 Eco-mode™ 脉冲跳跃
- 的低关断电流（低于 10μA）
- 1% 反馈电压精度 (25°C)
- 从预偏置输出电压中启动
- 逐周期断续过流限制
- 非锁存过压保护 (OVP)，欠压闭锁 (UVLO) 和热关断 (TSD) 保护
- 固定软启动时间：1ms

2 应用

- 数字电视电源
- 高清 Blu-ray Disc™ 播放器
- 网络家庭终端设备
- 数字机顶盒 (STB)

4 简化电路原理图



3 说明

TPS562200 和 TPS563200 是简单且易于使用的 2A/3A 同步降压转换器，它们均采用 SOT-23 封装。

此器件被优化为使用尽可能少的外部组件即可运行，并且可以实现低待机电流。

这些开关模式电源 (SMPS) 器件采用 D-CAP2 模式控制，从而提供快速瞬态响应，并且在无需外部补偿组件的情况下支持诸如高分子聚合物等低等效串联电阻 (ESR) 输出电容器以及超低 ESR 陶瓷电容器。

TPS562200 和 TPS563200 可在高级 Eco-mode 下运行，从而能在轻载运行期间保持高效率。此类器件采用 6 引脚 1.6mm x 2.9mm SOT (DDC) 封装，工作环境温度范围为 -40°C 到 85°C。

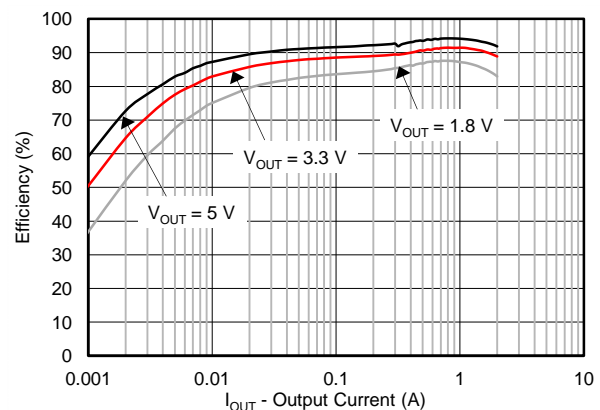
器件信息⁽¹⁾

部件号	封装	封装尺寸 (标称值)
TPS562200	SOT (6)	1.60mm x 2.90mm
TPS563200 ⁽²⁾		

(1) 如需了解所有可用封装，请见数据表末尾的可订购产品附录。

(2) 产品预览

TPS562200 效率



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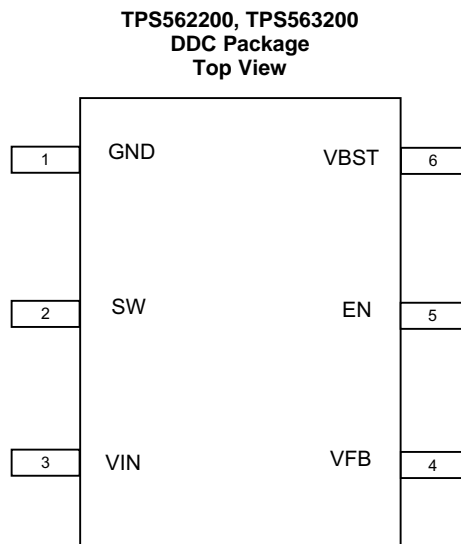
5 修订历史记录

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision A (January 2014) to Revision B	Page
• 数据表标题从: 4.5V 至 17V 输入, 2A 同步降压.. 更改为: 4.5V 至 17V 输入, 2A/3A 同步降压	1
• 更改了数据表以符合最新的 Ti 格式	1
• 器件编号从 TPS563209 更改为 TPS563200	1
• 已添加特性: 集成 68mΩ 和 39mΩ FET ('563200)	1
• 已将特性从: 2% 反馈电压精度 (25°C) 更改为: 1% 反馈电压精度 (25°C)	1
• Added the Timing Requirements table	5
• Added Table 1	13
• Changed Table 2	13
• Deleted sentence following Table 2 "For higher output voltages, additional phase boost can be achieved by adding a feed forward capacitor (C7) in parallel with R2."	14
• Added Application Information for the TPS563200 device	17
• Added Table 3	17

Changes from Original (January 2014) to Revision A	Page
• 器件状态从: 产品预览更改为: 生产	1

6 Pin Configuration and Functions



Pin Functions

PIN		DESCRIPTION
NAME	NUMBER	
GND	1	Ground pin Source terminal of low-side power NFET as well as the ground terminal for controller circuit. Connect sensitive VFB to this GND at a single point.
SW	2	Switch node connection between high-side NFET and low-side NFET.
VIN	3	Input voltage supply pin. The drain terminal of high-side power NFET.
VFB	4	Converter feedback input. Connect to output voltage with feedback resistor divider.
EN	5	Enable input control. Active high and must be pulled up to enable the device.
VBST	6	Supply input for the high-side NFET gate drive circuit. Connect a 0.1µF capacitor between VBST and SW pins.

7 Specifications

7.1 Absolute Maximum Ratings⁽¹⁾

over operating free-air temperature range (unless otherwise noted)

		VALUE		UNIT
		MIN	MAX	
Input voltage range	VIN, EN	-0.3	19	V
	VBST	-0.3	25	V
	VBST (10 ns transient)	-0.3	27	V
	VBST (vs SW)	-0.3	6.5	V
	VFB	-0.3	6.5	V
	SW	-2	19	V
	SW (10 ns transient)	-3.5	21	V
Operating junction temperature, T _J		-40	150	°C

- (1) Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

7.2 Handling Ratings

			MIN	MAX	UNIT
T _{stg}	Storage temperature range		-55	150	°C
V _(ESD)	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins ⁽¹⁾	-2	2	kV
		Charged device model (CDM), per JEDEC specification JESD22-C101, all pins ⁽²⁾	-500	500	V

- (1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

- (2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

			MIN	MAX	UNIT
V _{IN}	Supply input voltage range		4.5	17	V
V _I	Input voltage range	VBST	-0.1	23	V
		VBST (10 ns transient)	-0.1	26	
		VBST(vs SW)	-0.1	6	
		EN	-0.1	17	
		VFB	-0.1	5.5	
		SW	-1.8	17	
		SW (10 ns transient)	-3.5	20	
T _A	Operating free-air temperature		-40	85	°C

7.4 Thermal Information

THERMAL METRIC ⁽¹⁾		TPS562200	TPS563200	UNITS
		DDC (6 PINS)	DDC (6 PINS)	
R _{θJA}	Junction-to-ambient thermal resistance	109.2	87.9	°C/W
R _{θJctop}	Junction-to-case (top) thermal resistance	44.5	42.2	
R _{θJB}	Junction-to-board thermal resistance	57.3	13.6	
Ψ _{JT}	Junction-to-top characterization parameter	2.3	1.9	
Ψ _{JB}	Junction-to-board characterization parameter	60.4	13.3	

- (1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, SPRA953.

7.5 Electrical Characteristics

over operating free-air temperature range, $V_{IN} = 12V$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
SUPPLY CURRENT							
$I_{(VIN)}$	Operating – non-switching supply current	V_{IN} current, $T_A = 25^\circ C$, $EN = 5V$, $V_{FB} = 0.8V$	TPS562200	230	330	μA	
			TPS563200	190	290		
$I_{(VINS\overline{SDN})}$	Shutdown supply current	V_{IN} current, $T_A = 25^\circ C$, $EN = 0V$		3	10	μA	
LOGIC THRESHOLD							
$V_{EN(H)}$	EN high-level input voltage	EN	1.6			V	
$V_{EN(L)}$	EN low-level input voltage	EN			0.6	V	
R_{EN}	EN pin resistance to GND	$V_{EN} = 12V$	225	450	900	k Ω	
V_{FB} VOLTAGE AND DISCHARGE RESISTANCE							
$V_{FB(TH)}$	V_{FB} threshold voltage	$T_A = 25^\circ C$, $V_O = 1.05V$, $I_O = 10mA$, Eco-mode™ operation		772		mV	
		$T_A = 25^\circ C$, $V_O = 1.05V$, continuous mode operation	758	765	772	mV	
$I_{(VFB)}$	V_{FB} input current	$V_{FB} = 0.8V$, $T_A = 25^\circ C$		0	± 0.1	μA	
MOSFET							
$R_{DS(on)h}$	High side switch resistance	$T_A = 25^\circ C$, $V_{BST} - SW = 5.5V$	TPS562200	122		m Ω	
			TPS563200	68		m Ω	
$R_{DS(on)l}$	Low side switch resistance	$T_A = 25^\circ C$	TPS562200	72		m Ω	
			TPS563200	39		m Ω	
CURRENT LIMIT							
I_{oc1}	Current limit ⁽¹⁾	DC current, $V_{OUT} = 1.05V$, $L_{OUT} = 2.2\mu F$	TPS562200	2.5	3.2	4.3	A
			TPS563200	3.5	4.2	5.3	A
THERMAL SHUTDOWN							
T_{SDN}	Thermal shutdown threshold ⁽¹⁾	Shutdown temperature		155		$^\circ C$	
		Hysteresis		35			
OUTPUT UNDERVOLTAGE AND OVERVOLTAGE PROTECTION							
V_{OVP}	Output OVP threshold	OVP Detect ($L > H$)		125%			
V_{UVP}	Output Hiccup threshold	Hiccup detect ($H > L$)		65%			
$t_{UV\overline{PEN}}$	Output Hiccup enable delay	Relative to soft-start time		x1.7			
UVLO							
UVLO	UVLO threshold	Wake up V_{IN} voltage	3.45	3.75	4.05	V	
		Hysteresis V_{IN} voltage	0.13	0.32	0.55		

(1) Not production tested

7.6 Timing Requirements

		MIN	TYP	MAX	UNIT	
ON-TIME TIMER CONTROL						
t_{ON}	On time	$V_{IN} = 12V$, $V_O = 1.05V$	150		ns	
$t_{OFF(MIN)}$	Minimum off time	$T_A = 25^\circ C$, $V_{FB} = 0.5V$	260	310	ns	
SOFT START						
t_{ss}	Soft-start time	Internal soft-start time	0.7	1	1.3	ms

7.7 Typical Characteristics TPS562200

$V_{IN} = 12\text{ V}$ (unless otherwise noted).

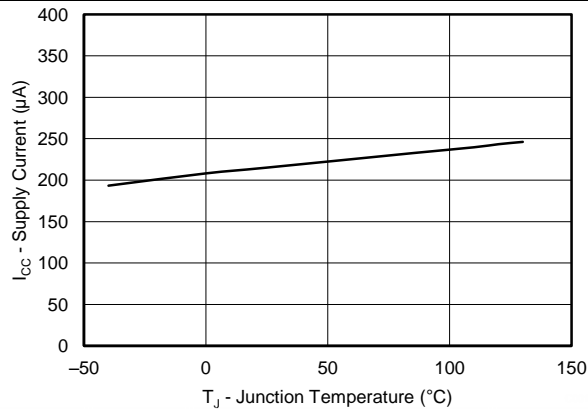


Figure 1. Supply Current vs Junction Temperature

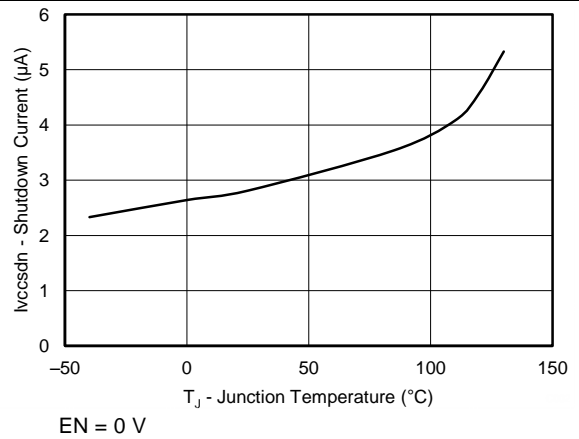


Figure 2. VIN Shutdown Current vs Junction Temperature

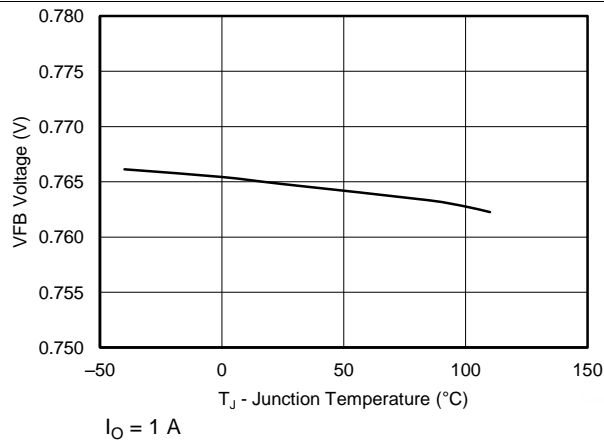


Figure 3. VFB Voltage vs Junction Temperature

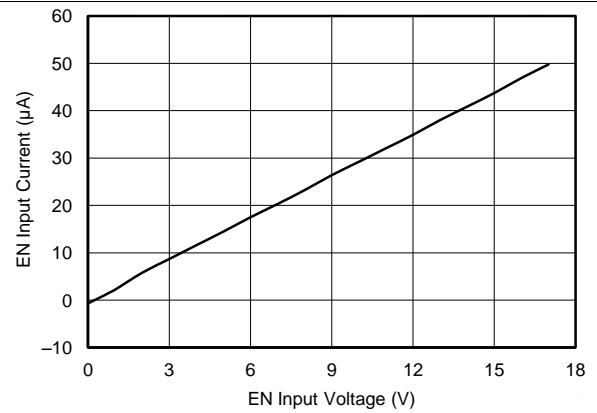


Figure 4. EN Current vs EN Voltage

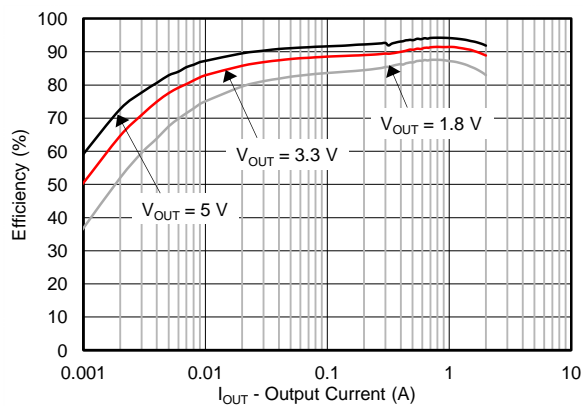


Figure 5. Efficiency vs Output Current

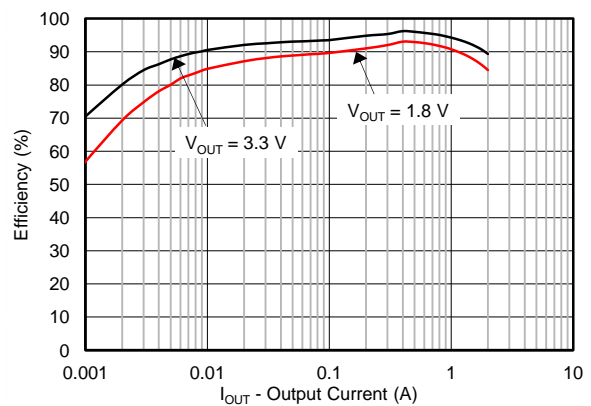


Figure 6. Efficiency vs Output Current ($V_{IN} = 5\text{ V}$)

Typical Characteristics TPS562200 (continued)

$V_{IN} = 12\text{ V}$ (unless otherwise noted).

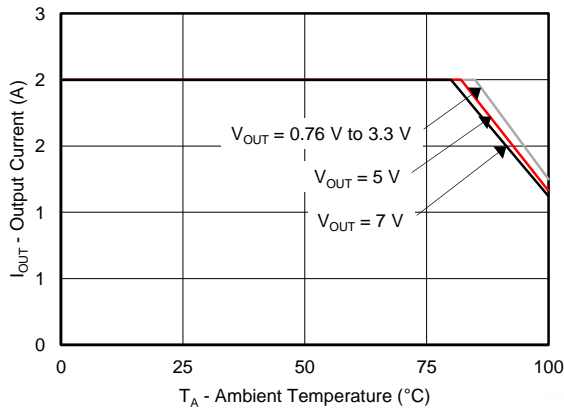


Figure 7. Output Current vs Ambient Temperature

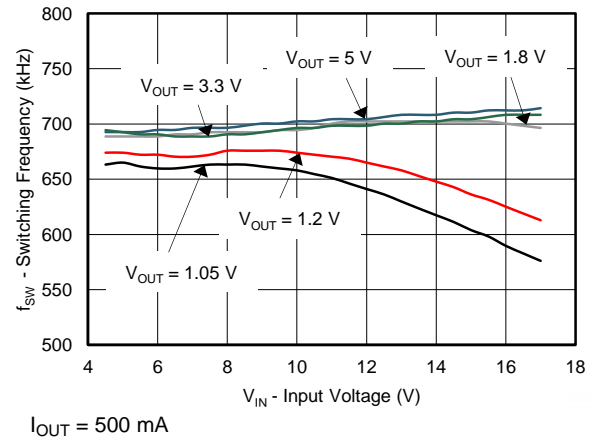


Figure 8. Switching Frequency vs Input Voltage

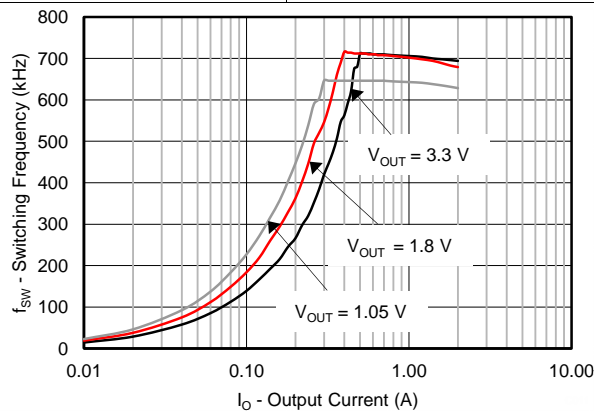
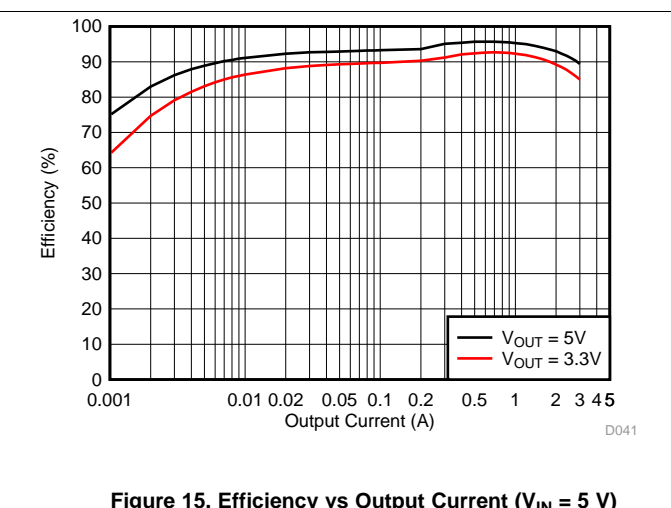
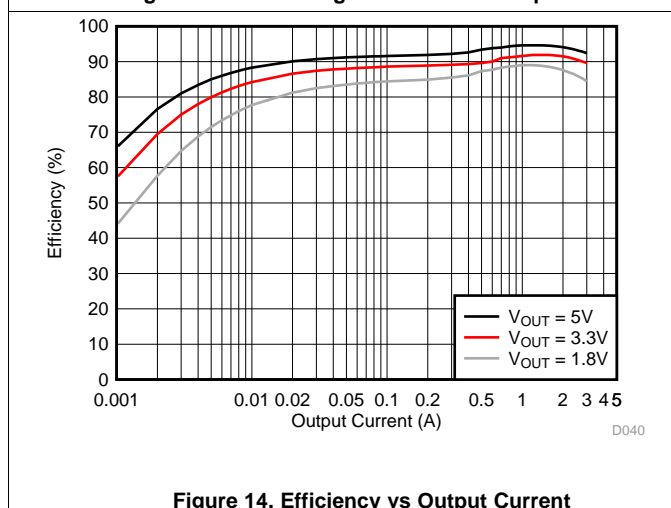
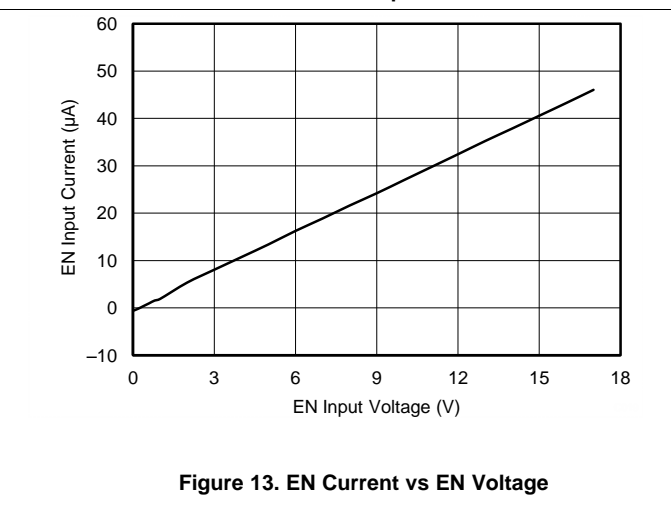
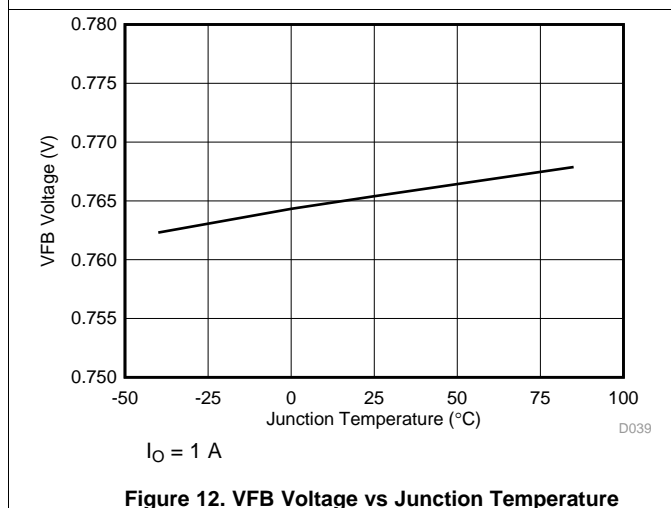
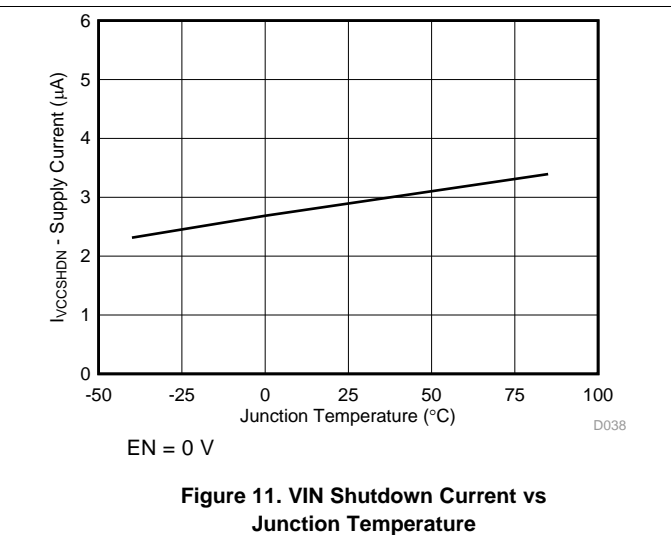
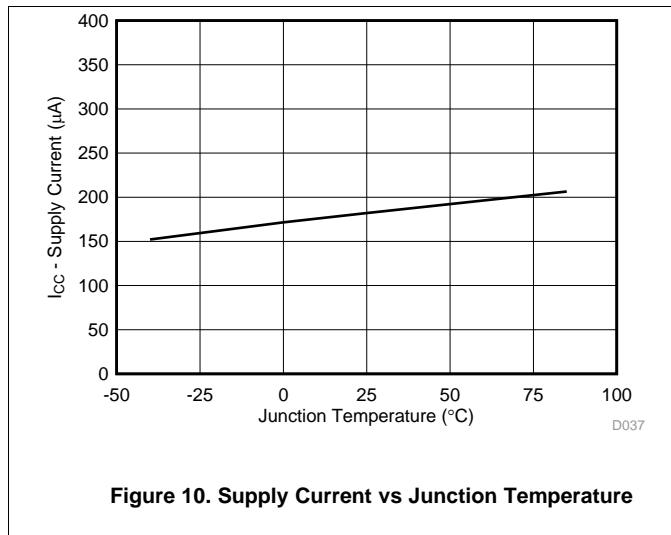


Figure 9. Switching Frequency vs Output Current

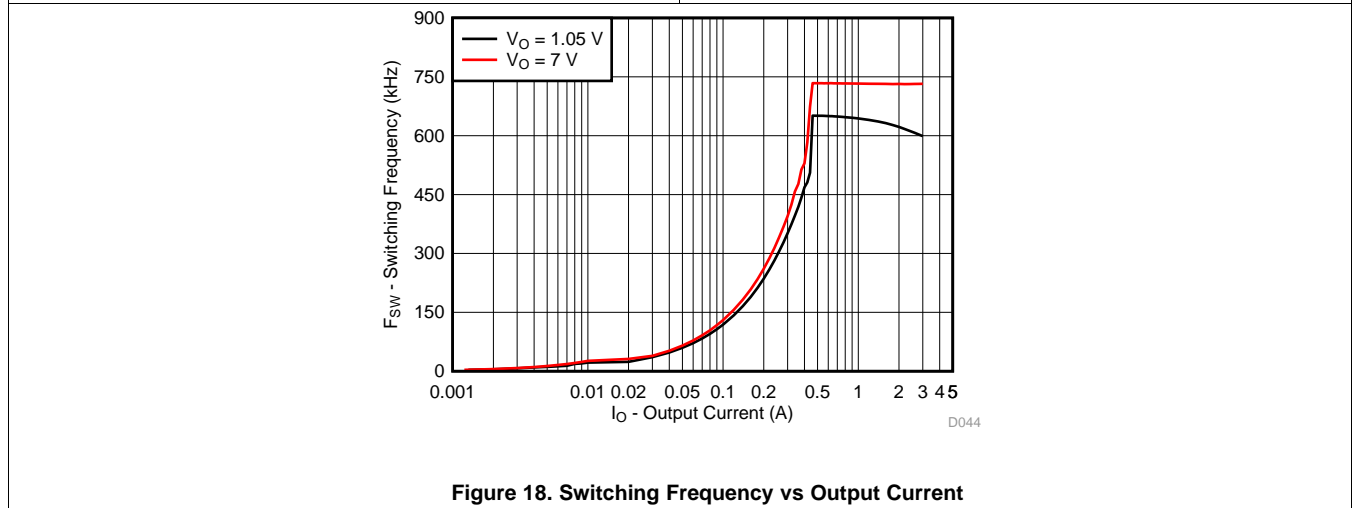
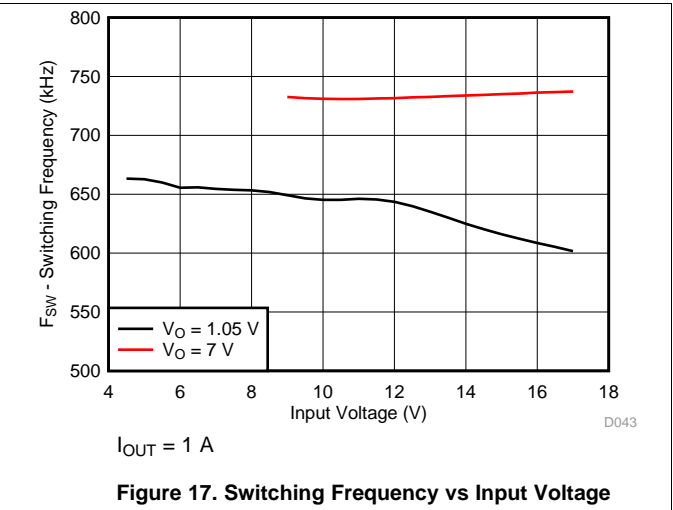
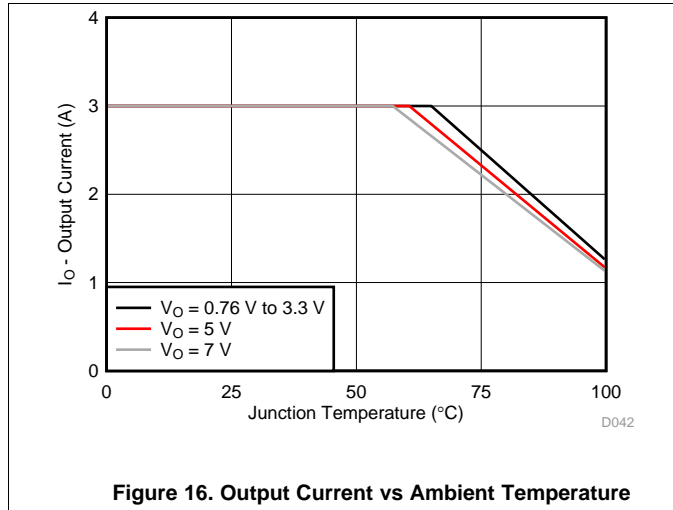
7.8 Typical Characteristics TPS563200

$V_{IN} = 12\text{ V}$ (unless otherwise noted).



Typical Characteristics TPS563200 (continued)

$V_{IN} = 12\text{ V}$ (unless otherwise noted).



8 Detailed Description

8.1 Overview

The TPS562200 and TPS563200 are 2-A and 3-A synchronous step-down converters. The proprietary D-CAP2™ mode control supports low ESR output capacitors such as specialty polymer capacitors and multi-layer ceramic capacitors without complex external compensation circuits. The fast transient response of D-CAP2™ mode control can reduce the output capacitance required to meet a specific level of performance.

8.2 Functional Block Diagrams

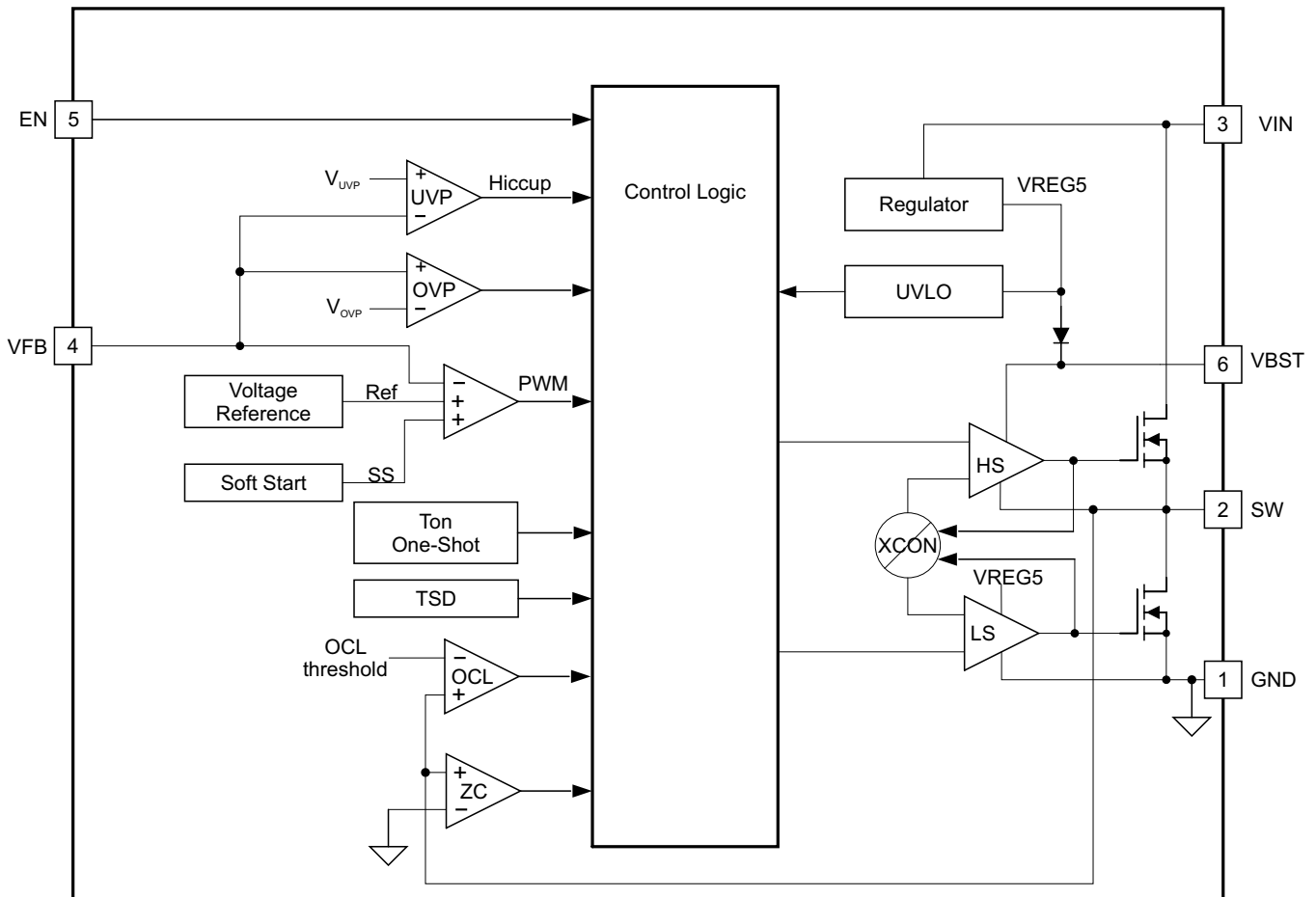


Figure 19. Functional Block Diagram: TPS562200 and TPS563200

8.3 Feature Description

8.3.1 The Adaptive On-Time Control and PWM Operation

The main control loop of the TPS562200 and TPS563200 are adaptive on-time pulse width modulation (PWM) controller that supports a proprietary D-CAP2™ mode control. The D-CAP2™ mode control combines adaptive on-time control with an internal compensation circuit for pseudo-fixed frequency and low external component count configuration with both low ESR and ceramic output capacitors. It is stable even with virtually no ripple at the output.

At the beginning of each cycle, the high-side MOSFET is turned on. This MOSFET is turned off after internal one shot timer expires. This one shot duration is set proportional to the converter input voltage, V_{IN} , and inversely proportional to the output voltage, V_O , to maintain a pseudo-fixed frequency over the input voltage range, hence it is called adaptive on-time control. The one-shot timer is reset and the high-side MOSFET is turned on again when the feedback voltage falls below the reference voltage. An internal ramp is added to reference voltage to simulate output ripple, eliminating the need for ESR induced output ripple from D-CAP2™ mode control.

8.3.2 Advanced Eco-Mode™ Control

The TPS562200 and TPS563200 are designed with Advanced Eco-mode™ to maintain high light load efficiency. As the output current decreases from heavy load condition, the inductor current is also reduced and eventually comes to point that its rippled valley touches zero level, which is the boundary between continuous conduction and discontinuous conduction modes. The rectifying MOSFET is turned off when the zero inductor current is detected. As the load current further decreases, the converter runs into discontinuous conduction mode. The on-time is kept almost the same as it was in the continuous conduction mode so that it takes longer time to discharge the output capacitor with smaller load current to the level of the reference voltage. This makes the switching frequency lower, proportional to the load current, and keeps the light load efficiency high. The transition point to the light load operation $I_{OUT(LL)}$ current can be calculated in [Equation 1](#).

$$I_{OUT(LL)} = \frac{1}{2 \times L \times f_{SW}} \times \frac{(V_{IN} - V_{OUT}) \times V_{OUT}}{V_{IN}} \quad (1)$$

8.3.3 Soft Start and Pre-Biased Soft Start

The TPS562200 and TPS563200 have an internal 1 ms soft-start. When the EN pin becomes high, the internal soft-start function begins ramping up the reference voltage to the PWM comparator. If the output capacitor is pre-biased at startup, the devices initiate switching and start ramping up only after the internal reference voltage becomes greater than the feedback voltage VFB. This scheme ensures that the converters ramp up smoothly into regulation point.

8.3.4 Current Protection

The output overcurrent limit (OCL) is implemented using a cycle-by-cycle valley detect control circuit. The switch current is monitored during the OFF state by measuring the low-side FET drain to source voltage. This voltage is proportional to the switch current. To improve accuracy, the voltage sensing is temperature compensated.

During the on time of the high-side FET switch, the switch current increases at a linear rate determined by V_{IN} , V_{OUT} , the on-time and the output inductor value. During the on time of the low-side FET switch, this current decreases linearly. The average value of the switch current is the load current I_{OUT} . If the monitored current is above the OCL level, the converter maintains low-side FET on and delays the creation of a new set pulse, even the voltage feedback loop requires one, until the current level becomes OCL level or lower. In subsequent switching cycles, the on-time is set to a fixed value and the current is monitored in the same manner. If the over current condition exists consecutive switching cycles, the internal OCL threshold is set to a lower level, reducing the available output current. When a switching cycle occurs where the switch current is not above the lower OCL threshold, the counter is reset and the OCL threshold is returned to the higher value.

There are some important considerations for this type of over-current protection. The load current is higher than the over-current threshold by one half of the peak-to-peak inductor ripple current. Also, when the current is being limited, the output voltage tends to fall as the demanded load current may be higher than the current available from the converter. This may cause the output voltage to fall. When the VFB voltage falls below the UVP threshold voltage, the UVP comparator detects it. Then, the device shuts down after the UVP delay time (typically 14 μ s) and re-start after the hiccup time (typically 12 ms).

Feature Description (continued)

When the overcurrent condition is removed, the output voltage returns to the regulated value.

8.3.5 Over Voltage Protection

TPS562200 and TPS563200 detect overvoltage condition by monitoring the feedback voltage (VFB). When the feedback voltage becomes higher than 125% of the target voltage, the OVP comparator output goes high and both the high-side MOSFET driver and the low-side MOSFET driver turn off. This function is non-latch operation.

8.3.6 UVLO Protection

Undervoltage lock out protection (UVLO) monitors the internal regulator voltage. When the voltage is lower than UVLO threshold voltage, the device is shut off. This protection is non-latching.

8.3.7 Thermal Shutdown

The device monitors the temperature of itself. If the temperature exceeds the threshold value (typically 155°C), the device is shut off. This is a non-latch protection.

8.4 Device Functional Modes

8.4.1 Normal Operation

When the input voltage is above the UVLO threshold and the EN voltage is above the enable threshold, the TPS562200 and TPS563200 can operate in their normal switching modes. Normal continuous conduction mode (CCM) occurs when the minimum switch current is above 0 A. In CCM, the TPS562200 and TPS563200 operate at a quasi-fixed frequency of 650 kHz.

8.4.2 Eco-mode Operation

When the TPS562200 and TPS563200 are in the normal CCM operating mode and the switch current falls to 0 A, the TPS562200 and TPS563200 begin operating in pulse skipping eco-mode. Each switching cycle is followed by a period of energy saving sleep time. The sleep time ends when the VFB voltage falls below the eco-mode threshold voltage. As the output current decreases the perceived time between switching pulses increases.

8.4.3 Standby Operation

When the TPS562200 and TPS563200 are operating in either normal CCM or eco-mode, they may be placed in standby by asserting the EN pin low.

9 Application and Implementation

9.1 Application Information

The TPS562200 and TPS563200 are typically used as step down converters, which convert a voltage from 4.5V - 17V to a lower voltage. Webench software is available to aid in the design and analysis of circuits

9.2 Typical Applications

9.2.1 TPS562200 4.5-V to 17-V Input, 1.05-V Output Converter

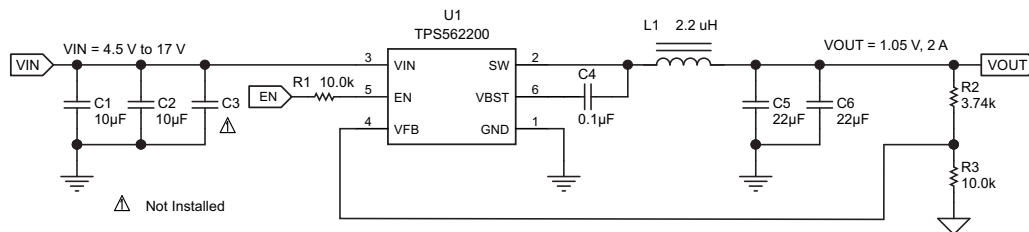


Figure 20. TPS562200 1.05V/2A Reference Design

9.2.1.1 Design Requirements

To begin the design process, the user must know a few application parameters:

Table 1. Design Parameters

PARAMETER	VALUE
Input voltage range	4.5 V to 17V
Output voltage	1.05V
Output current	2A
Output voltage ripple	20mVpp

9.2.1.2 Detailed Design Procedures

9.2.1.2.1 Output Voltage Resistors Selection

The output voltage is set with a resistor divider from the output node to the VFB pin. It is recommended to use 1% tolerance or better divider resistors. Start by using Equation 2 to calculate V_{OUT} .

To improve efficiency at light loads consider using larger value resistors, too high of resistance will be more susceptible to noise and voltage errors from the VFB input current will be more noticeable.

$$V_{OUT} = 0.765 \times \left(1 + \frac{R2}{R3} \right) \quad (2)$$

9.2.1.2.2 Output Filter Selection

The LC filter used as the output filter has double pole at:

$$F_P = \frac{1}{2\pi\sqrt{L_{OUT} \times C_{OUT}}} \quad (3)$$

At low frequencies, the overall loop gain is set by the output set-point resistor divider network and the internal gain of the device. The low frequency phase is 180 degrees. At the output filter pole frequency, the gain rolls off at a -40 dB per decade rate and the phase drops rapidly. D-CAP2™ introduces a high frequency zero that reduces the gain roll off to -20 dB per decade and increases the phase to 90 degrees one decade above the zero frequency. The inductor and capacitor selected for the output filter must be selected so that the double pole of Equation 3 is located below the high frequency zero but close enough that the phase boost provided by the high frequency zero provides adequate phase margin for a stable circuit. To meet this requirement use the values recommended in Table 1.

Table 2. TPS562200 Recommended Component Values

Output Voltage (V)	R2 (kΩ)	R3 (kΩ)	L1 (μH) TPS562200			C8 + C9 (μF)
			MIN	TYP	MAX	
1	3.09	10.0	1.5	2.2	4.7	20 - 68
1.05	3.74	10.0	1.5	2.2	4.7	20 - 68
1.2	5.76	10.0	1.5	2.2	4.7	20 - 68
1.5	9.53	10.0	1.5	2.2	4.7	20 - 68
1.8	13.7	10.0	1.5	2.2	4.7	20 - 68
2.5	22.6	10.0	2.2	3.3	4.7	20 - 68
3.3	33.2	10.0	2.2	3.3	4.7	20 - 68
5	54.9	10.0	3.3	4.7	4.7	20 - 68
6.5	75	10.0	3.3	4.4	4.7	20 - 68

The inductor peak-to-peak ripple current, peak current and RMS current are calculated using [Equation 4](#), [Equation 5](#) and [Equation 6](#). The inductor saturation current rating must be greater than the calculated peak current and the RMS or heating current rating must be greater than the calculated RMS current. Use 650 kHz for f_{SW} .

Use 650 kHz for f_{SW} . Make sure the chosen inductor is rated for the peak current of [Equation 5](#) and the RMS current of [Equation 6](#).

$$I_{P-P} = \frac{V_{OUT}}{V_{IN(MAX)}} \times \frac{V_{IN(MAX)} - V_{OUT}}{L_O \times f_{SW}} \quad (4)$$

$$I_{PEAK} = I_O + \frac{I_{P-P}}{2} \quad (5)$$

$$I_{LO(RMS)} = \sqrt{I_O^2 + \frac{1}{12} I_{P-P}^2} \quad (6)$$

For this design example, the calculated peak current is 2.34 A and the calculated RMS current is 2.01 A. The inductor used is a TDK CLF7045T-2R2N with a peak current rating of 5.5-A and an RMS current rating of 4.3-A

The capacitor value and ESR determines the amount of output voltage ripple. The device is intended for use with ceramic or other low ESR capacitors. Recommended values range from 20 μF to 68 μF. Use [Equation 7](#) to determine the required RMS current rating for the output capacitor.

$$I_{CO(RMS)} = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{\sqrt{12} \times V_{IN} \times L_O \times f_{SW}} \quad (7)$$

For this design two TDK C3216X5R0J226M 22 μF output capacitors are used. The typical ESR is 2 mΩ each. The calculated RMS current is 0.286 A and each output capacitor is rated for 4 A.

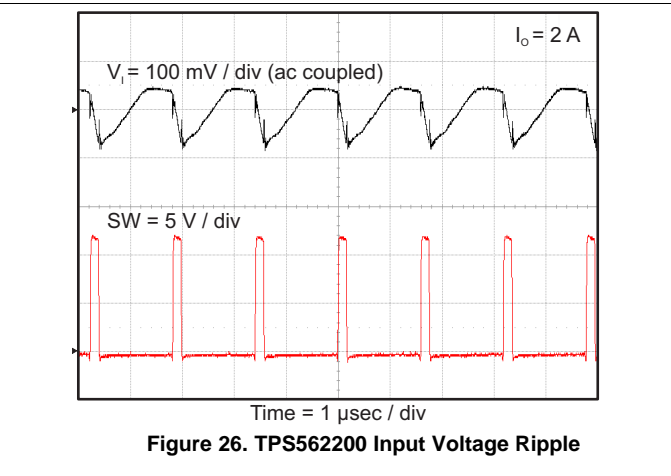
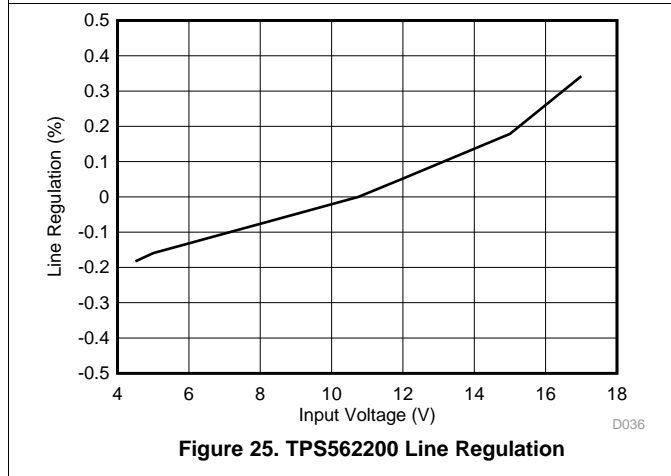
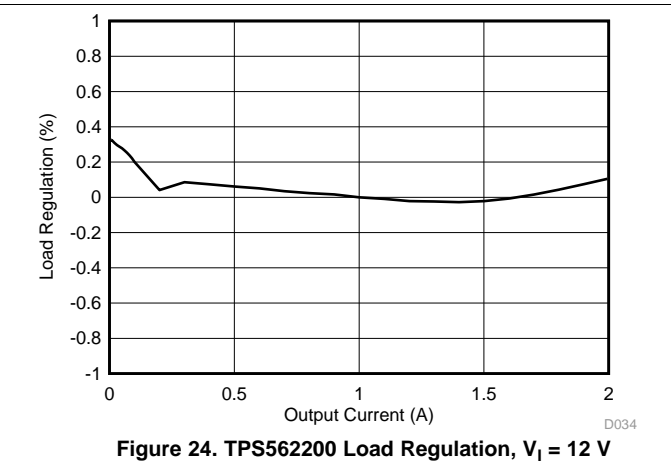
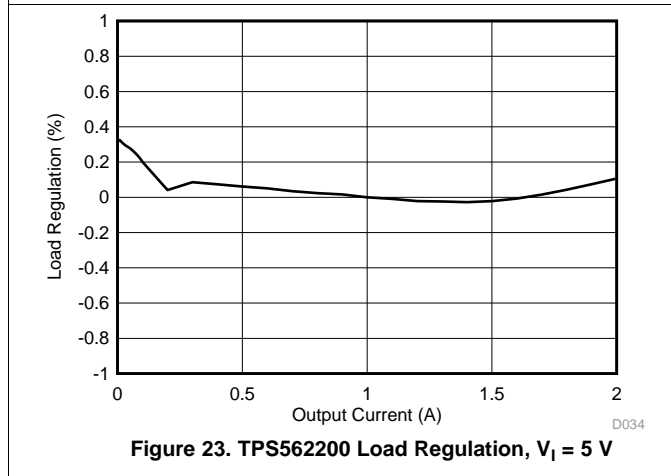
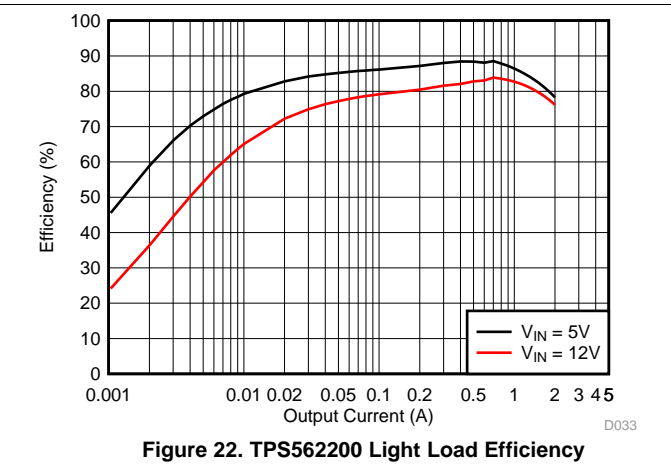
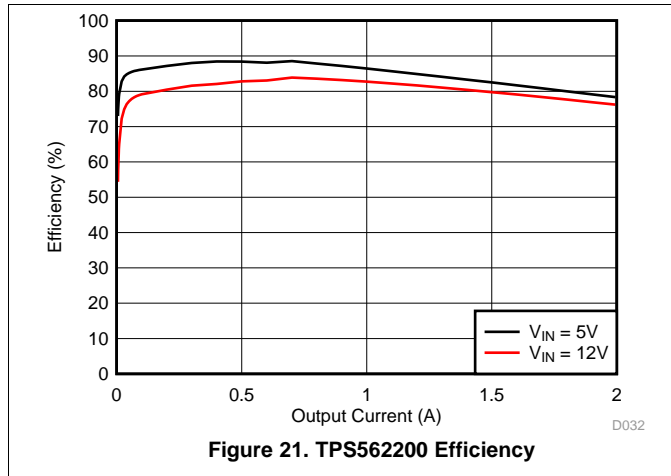
9.2.1.2.3 Input Capacitor Selection

The device requires an input decoupling capacitor and a bulk capacitor is needed depending on the application. A ceramic capacitor over 10 μF is recommended for the decoupling capacitor. An additional 0.1 μF capacitor(C3) from pin 3 to ground is optional to provide additional high frequency filtering. The capacitor voltage rating needs to be greater than the maximum input voltage.

9.2.1.2.4 Bootstrap Capacitor Selection

A 0.1 μF ceramic capacitor must be connected between the VBST to SW pin for proper operation. It is recommended to use a ceramic capacitor.

9.2.1.3 Application Curves



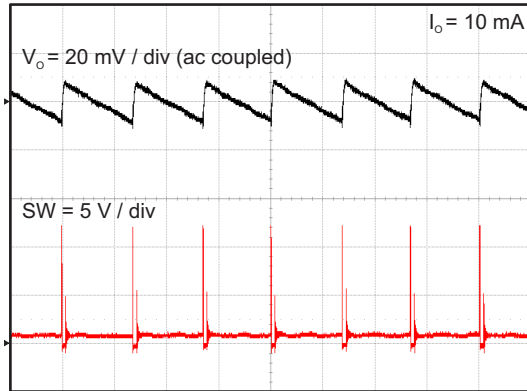


Figure 27. TPS562200 Output Voltage Ripple

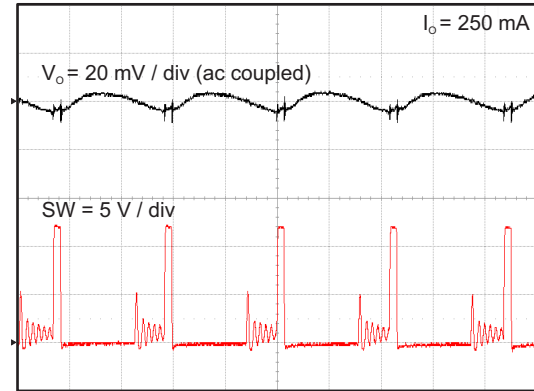


Figure 28. TPS562200 Output Voltage Ripple

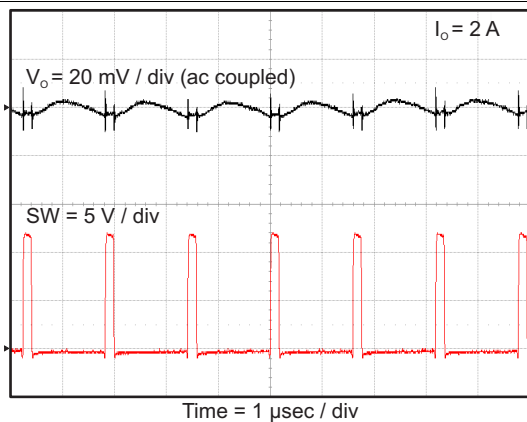


Figure 29. TPS562200 Output Voltage Ripple

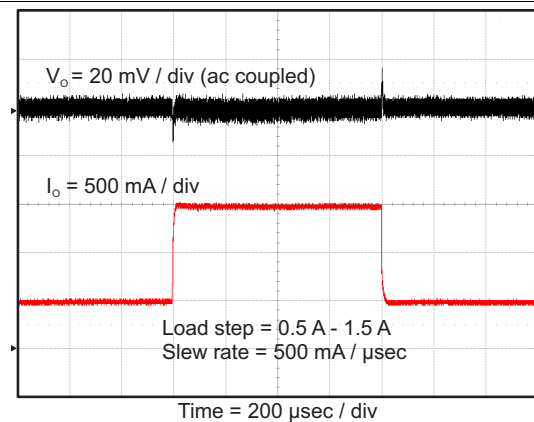


Figure 30. TPS562200 Transient Response

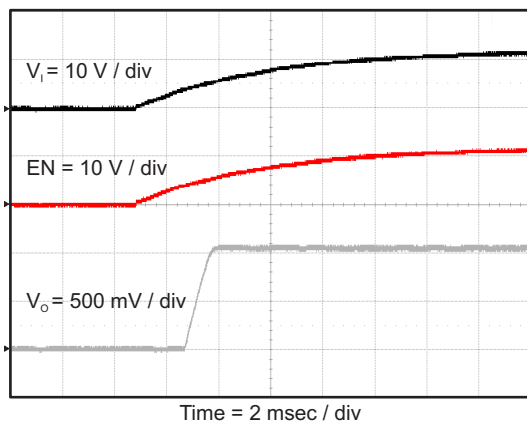


Figure 31. TPS562200 Start Up Relative to V_I

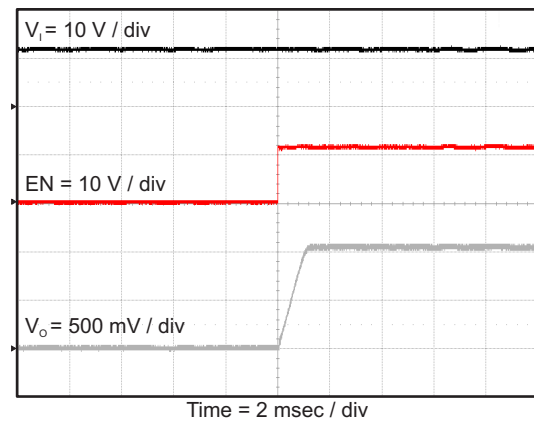


Figure 32. TPS562200 Start Up Relative to EN

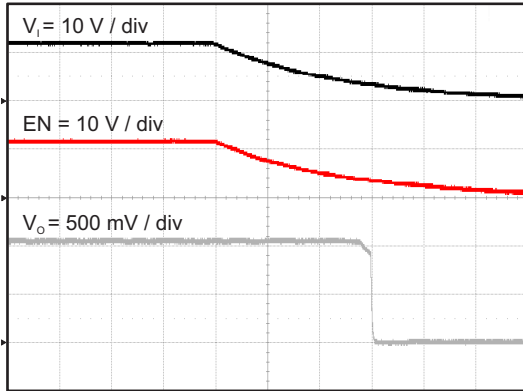


Figure 33. TPS562200 Shut Down Relative to V_i

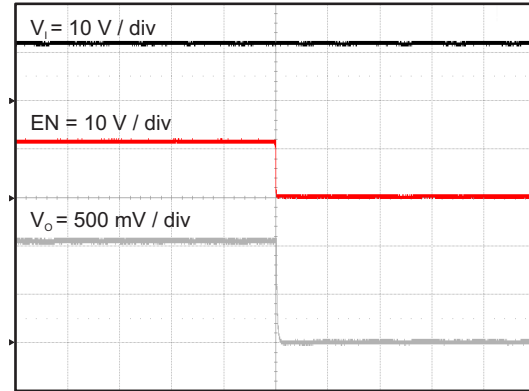


Figure 34. TPS562200 Shut Down Relative to EN

9.2.2 TPS563200 4.5-V to 17-V Input, 1.05-V Output Converter

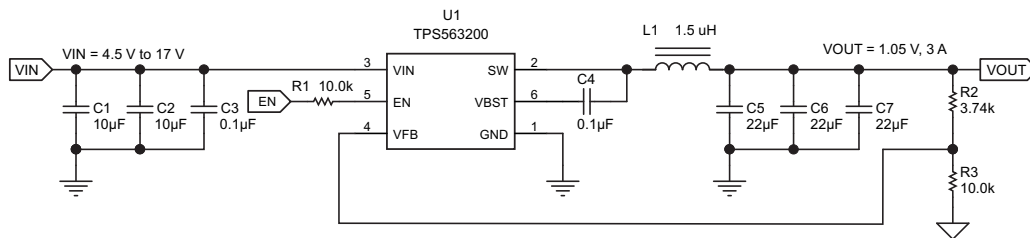


Figure 35. TPS563200 1.05V/3A Reference Design

9.2.2.1 Design Requirements

To begin the design process, the user must know a few application parameters:

Table 3. Design Parameters

PARAMETER	VALUE
Input voltage range	4.5 V to 17V
Output voltage	1.05V
Output current	3A
Output voltage ripple	20mVpp

9.2.2.2 Detailed Design Procedures

The detailed design procedure for TPS563200 is the same as for TPS562200 except for inductor selection.

9.2.2.2.1 Output Filter Selection
Table 4. TPS563200 Recommended Component Values

Output Voltage (V)	R2 (kΩ)	R3 (kΩ)	L1 (μH) TPS563200			C8 + C9 (μF)
			MIN	TYP	MAX	
1	3.09	10.0	1.0	1.5	4.7	20 - 68
1.05	3.74	10.0	1.0	1.5	4.7	20 - 68
1.2	5.76	10.0	1.0	1.5	4.7	20 - 68
1.5	9.53	10.0	1.0	1.5	4.7	20 - 68
1.8	13.7	10.0	1.5	2.2	4.7	20 - 68
2.5	22.6	10.0	1.5	2.2	4.7	20 - 68
3.3	33.2	10.0	1.5	2.2	4.7	20 - 68
5	54.9	10.0	2.2	3.3	4.7	20 - 68
6.5	75	10.0	2.2	3.3	4.7	20 - 68

The inductor peak-to-peak ripple current, peak current and RMS current are calculated using [Equation 8](#), [Equation 9](#) and [Equation 10](#). The inductor saturation current rating must be greater than the calculated peak current and the RMS or heating current rating must be greater than the calculated RMS current. Use 650 kHz for f_{SW} .

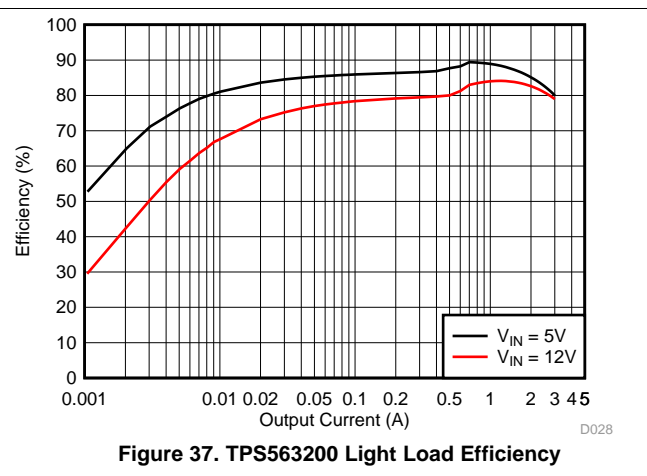
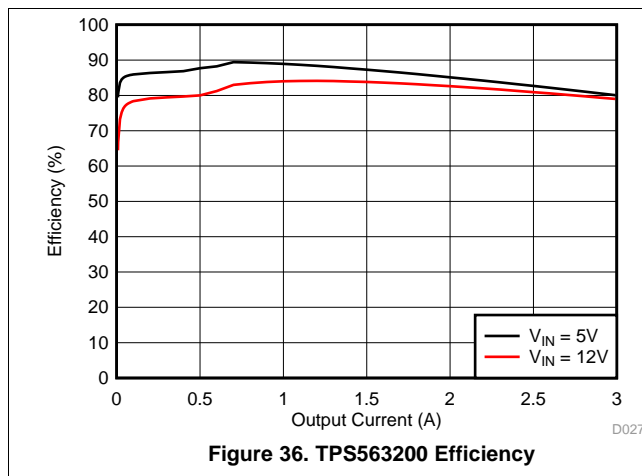
Use 650 kHz for f_{SW} . Make sure the chosen inductor is rated for the peak current of [Equation 9](#) and the RMS current of [Equation 10](#).

$$I_{P-P} = \frac{V_{OUT}}{V_{IN(MAX)}} \times \frac{V_{IN(MAX)} - V_{OUT}}{L_O \times f_{SW}} \quad (8)$$

$$I_{PEAK} = I_O + \frac{I_{P-P}}{2} \quad (9)$$

$$I_{LO(RMS)} = \sqrt{I_O^2 + \frac{1}{12} I_{P-P}^2} \quad (10)$$

For this design example, the calculated peak current is 3.505 A and the calculated RMS current is 3.014 A. The inductor used is a TDK CLF7045T-1R5N with a peak current rating of 7.3-A and an RMS current rating of 4.9-A

9.2.2.3 Application Curves


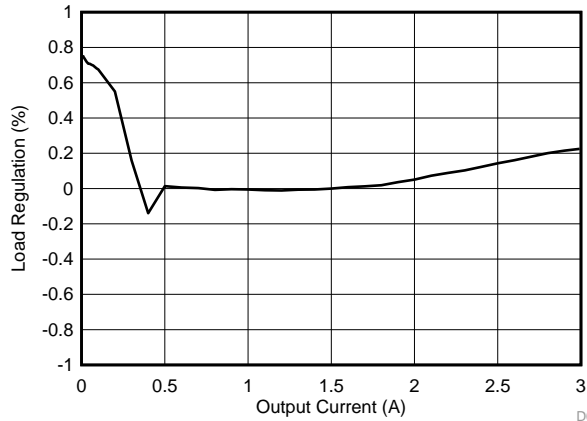


Figure 38. TPS563200 Load Regulation, $V_I = 5\text{ V}$

D029

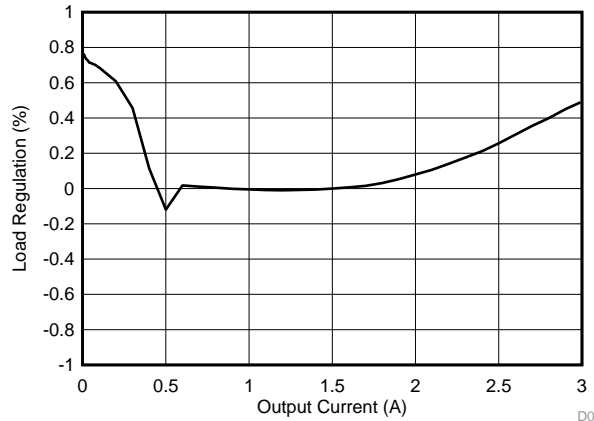


Figure 39. TPS563200 Load Regulation, $V_I = 12\text{ V}$

D030

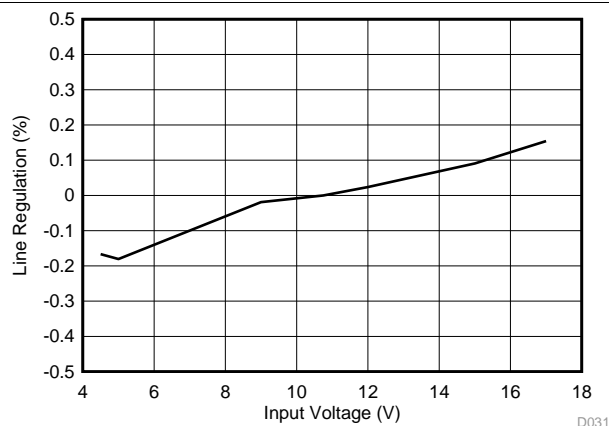


Figure 40. TPS563200 Line Regulation

D031

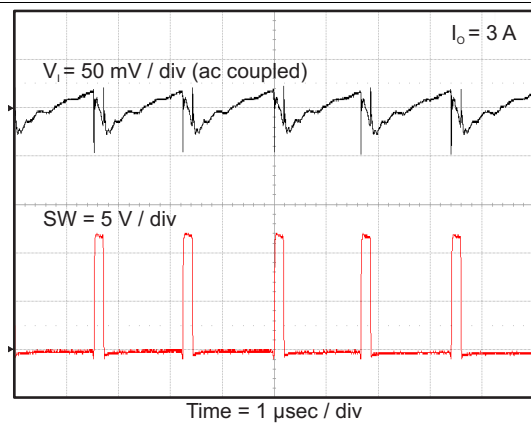


Figure 41. TPS563200 Input Voltage Ripple

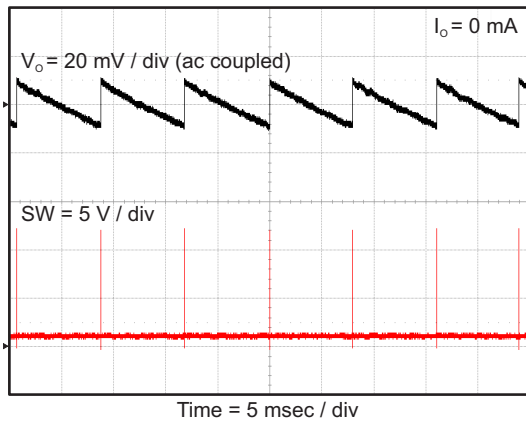


Figure 42. TPS563200 Output Voltage Ripple

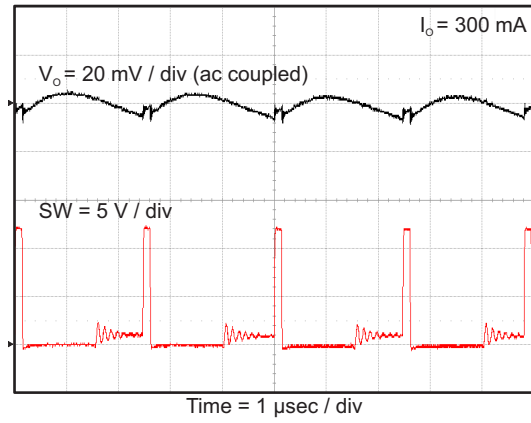


Figure 43. TPS563200 Output Voltage Ripple

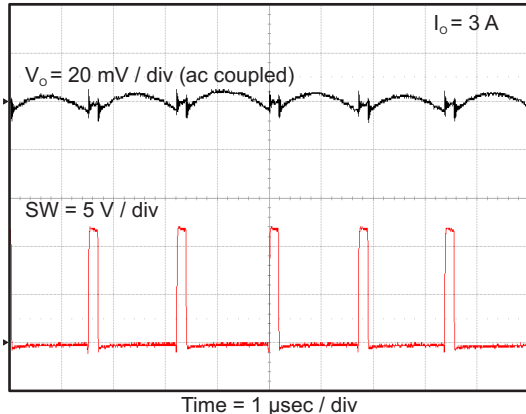


Figure 44. TPS563200 Output Voltage Ripple

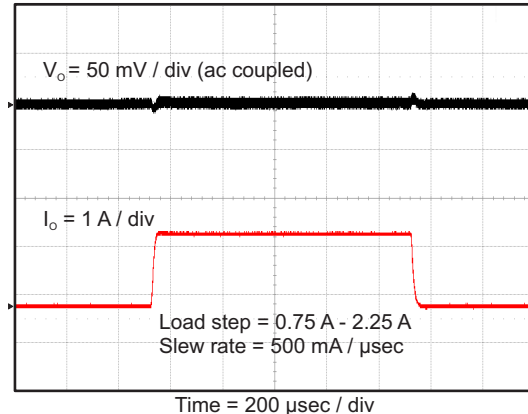


Figure 45. TPS563200 Transient Response

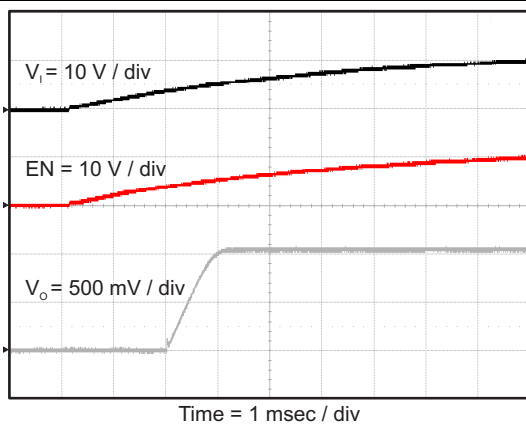


Figure 46. TPS563200 Start Up Relative to V_i

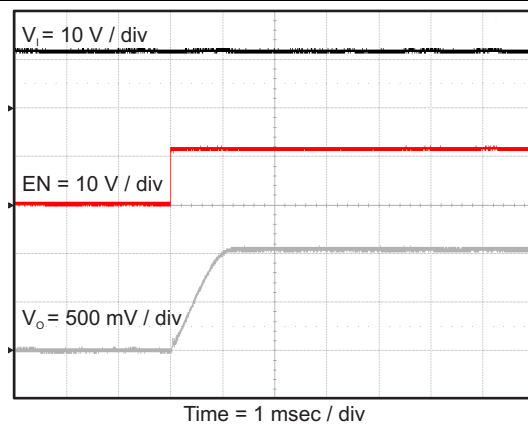


Figure 47. TPS563200 Start Up Relative to EN

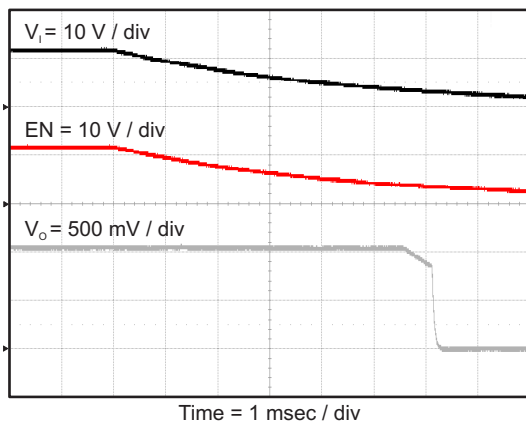


Figure 48. TPS563200 Shut Down Relative to V_i

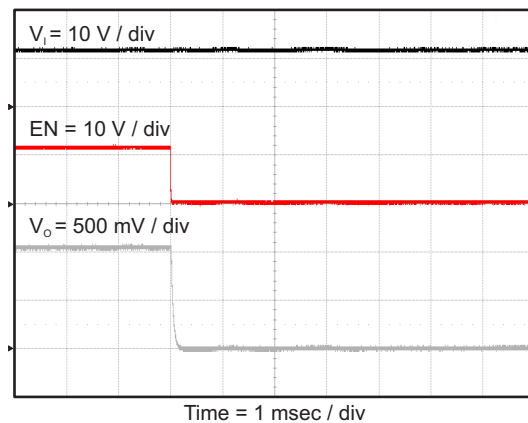


Figure 49. TPS563200 Shut Down Relative to EN

10 Power Supply Recommendations

The TPS562200 and TPS563200 are designed to operate from input supply voltage in the range of 4.5V to 17V. Buck converters require the input voltage to be higher than the output voltage for proper operation. The maximum recommended operating duty cycle is 65%. Using that criteria, the minimum recommended input voltage is $V_o / 0.65$.

11 Layout

11.1 Layout Guidelines

1. VIN and GND traces should be as wide as possible to reduce trace impedance. The wide areas are also of advantage from the view point of heat dissipation.
2. The input capacitor and output capacitor should be placed as close to the device as possible to minimize trace impedance.
3. Provide sufficient vias for the input capacitor and output capacitor.
4. Keep the SW trace as physically short and wide as practical to minimize radiated emissions.
5. Do not allow switching current to flow under the device.
6. A separate VOUT path should be connected to the upper feedback resistor
7. Make a Kelvin connection to the GND pin for the feedback path.
8. Voltage feedback loop should be placed away from the high-voltage switching trace, and preferably has ground shield.
9. The trace of the VFB node should be as small as possible to avoid noise coupling.
10. The GND trace between the output capacitor and the GND pin should be as wide as possible to minimize its trace impedance.

11.2 Layout Example

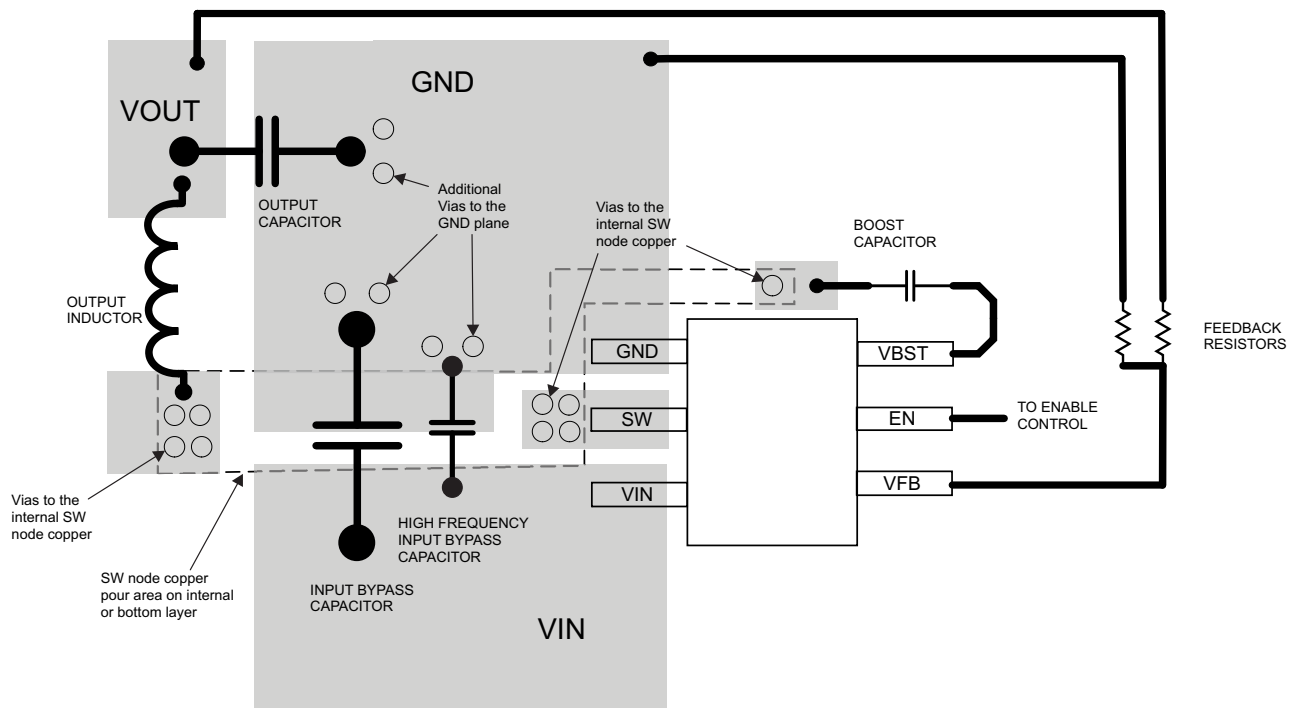


Figure 50. Typical Layout

12 器件和文档支持

12.1 相关链接

以下表格列出了快速访问链接。范围包括技术文档、支持与社区资源、工具和软件，并且可以快速访问样片或购买链接。

表 5. 相关链接

部件	产品文件夹	样片与购买	技术文档	工具与软件	支持与社区
TPS562200	请单击此处	请单击此处	请单击此处	请单击此处	请单击此处
TPS563200	请单击此处	请单击此处	请单击此处	请单击此处	请单击此处

12.2 商标

D-CAP2, Eco-mode are trademarks of Texas Instruments.
Blu-ray Disc is a trademark of Blu-ray Disc Association.

12.3 静电放电警告



这些装置包含有限的内置 ESD 保护。存储或装卸时，应将导线一起截短或将装置放置于导电泡棉中，以防止 MOS 门极遭受静电损伤。

12.4 术语表

[SLYZ022](#) — TI 术语表。

这份术语表列出并解释术语、首字母缩略词和定义。

13 机械封装和可订购信息

以下页中包括机械封装和可订购信息。 这些信息是针对指定器件可提供的最新数据。 这些数据会在无通知且不对本文档进行修订的情况下发生改变。 欲获得该数据表的浏览器版本，请查阅左侧的导航栏。

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放大器和线性器件	www.ti.com.cn/amplifiers	计算机及周边	www.ti.com.cn/computer
数据转换器	www.ti.com.cn/dataconverters	消费电子	www.ti.com.cn/consumer-apps
DLP® 产品	www.dlp.com	能源	www.ti.com.cn/energy
DSP - 数字信号处理器	www.ti.com.cn/dsp	工业应用	www.ti.com.cn/industrial
时钟和计时器	www.ti.com.cn/clockandtimers	医疗电子	www.ti.com.cn/medical
接口	www.ti.com.cn/interface	安防应用	www.ti.com.cn/security
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电源管理	www.ti.com.cn/power	视频和影像	www.ti.com.cn/video
微控制器 (MCU)	www.ti.com.cn/microcontrollers		
RFID 系统	www.ti.com.cn/rfidsys		
OMAP应用处理器	www.ti.com/omap		
无线连通性	www.ti.com.cn/wirelessconnectivity	德州仪器在线技术支持社区	www.deyisupport.com

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PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS562200DDCR	ACTIVE	SOT-23-THIN	DDC	6	3000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	200	Samples
TPS562200DDCT	ACTIVE	SOT-23-THIN	DDC	6	250	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	200	Samples
TPS563200DDCR	ACTIVE	SOT-23-THIN	DDC	6	3000	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	320	Samples
TPS563200DDCT	ACTIVE	SOT-23-THIN	DDC	6	250	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 125	320	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

Pb-Free (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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TAPE AND REEL INFORMATION



QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS562200DDCR	SOT-23-THIN	DDC	6	3000	180.0	9.5	3.17	3.1	1.1	4.0	8.0	Q3
TPS562200DDCT	SOT-23-THIN	DDC	6	250	180.0	9.5	3.17	3.1	1.1	4.0	8.0	Q3
TPS563200DDCR	SOT-23-THIN	DDC	6	3000	180.0	9.5	3.17	3.1	1.1	4.0	8.0	Q3
TPS563200DDCT	SOT-23-THIN	DDC	6	250	180.0	9.5	3.17	3.1	1.1	4.0	8.0	Q3

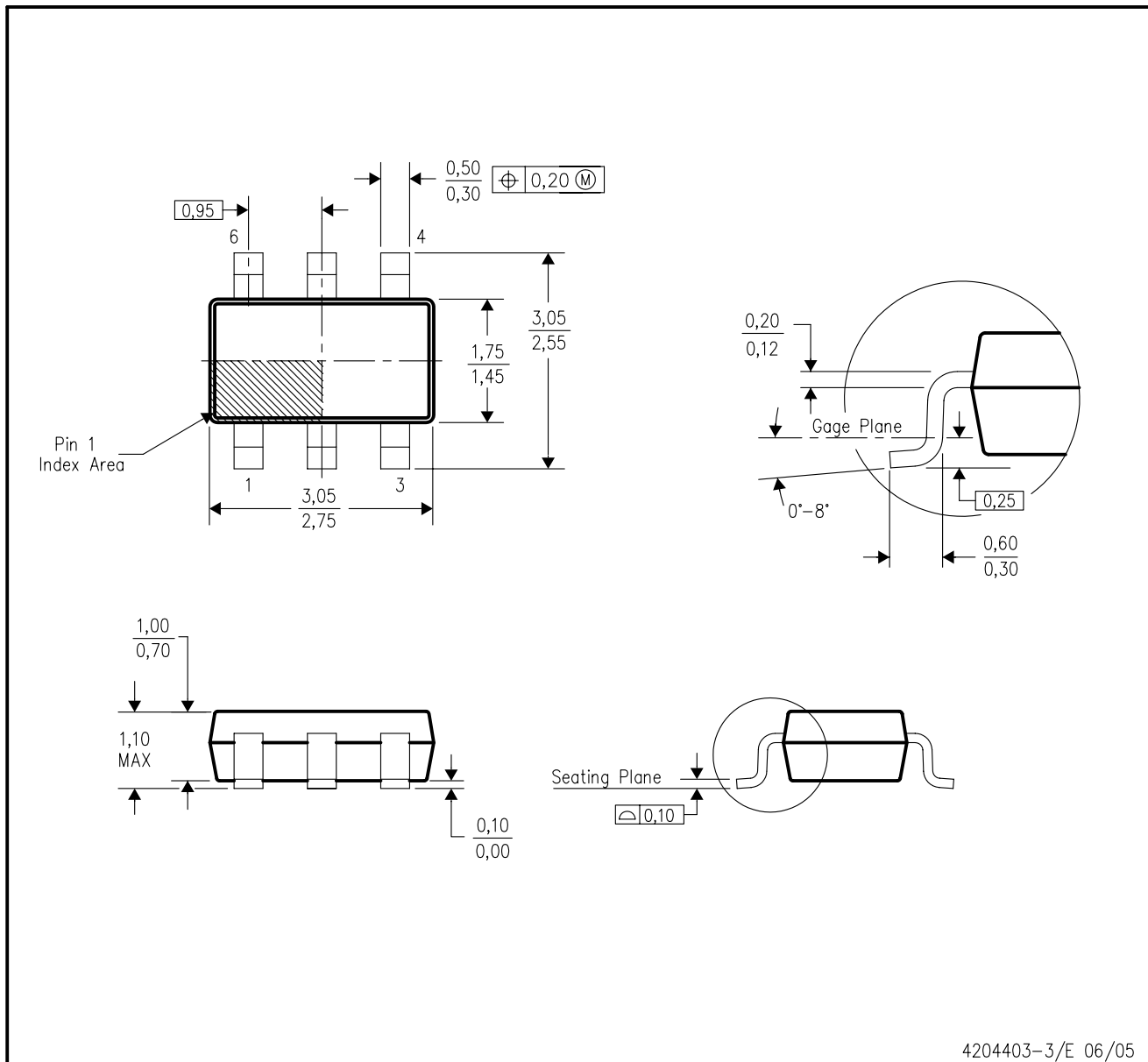
TAPE AND REEL BOX DIMENSIONS


*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS562200DDCR	SOT-23-THIN	DDC	6	3000	184.0	184.0	19.0
TPS562200DDCT	SOT-23-THIN	DDC	6	250	184.0	184.0	19.0
TPS563200DDCR	SOT-23-THIN	DDC	6	3000	184.0	184.0	19.0
TPS563200DDCT	SOT-23-THIN	DDC	6	250	184.0	184.0	19.0

DDC (R-PDSO-G6)

PLASTIC SMALL-OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
 - This drawing is subject to change without notice.
 - Body dimensions do not include mold flash or protrusion.
 - Falls within JEDEC MO-193 variation AA (6 pin).

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